

$$\frac{Y}{R} = \frac{\sum P_k \Delta_k}{\Delta}$$

$$P_1 = G_1 G_2 G_3$$

$$L_1 = -G_3 H$$

$$L_2 = G_2 G_3$$

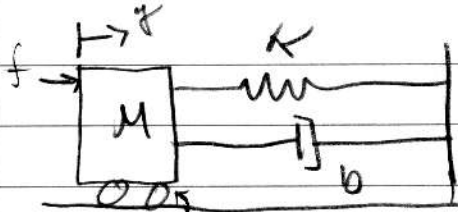
$$L_3 = -G_1 G_2 G_3$$

$$\Delta_1 = 1$$

$$\frac{Y}{R} = \frac{G_1 G_2 G_3}{1 - G_2 G_3 + G_3 H + G_1 G_2 G_3}$$

(60)

2)



assume no friction

FBD



Find Y/F

$M = 2.4 \text{ kg}$   $k = 30 \text{ N/m}$   $b = 10 \text{ Ns/m}$

No initial conditions

$$\frac{d^2 y}{dt^2} = s^2 Y(s) \quad \star$$

$$\frac{dy}{dt} = s Y(s)$$

$$M \frac{d^2 y}{dt^2} = F - ky - b \frac{dy}{dt}$$

$$M s^2 Y(s) = F(s) - k Y(s) - b s Y(s)$$

$$F(s) = Y(s) [M s^2 + k + b s]$$

$$\boxed{\frac{Y(s)}{F(s)} = \frac{1}{M s^2 + b s + k}} = \frac{1}{2.4 s^2 + 10 s + 30} = \frac{0.417}{s^2 + 4.17 s + 12.5}$$

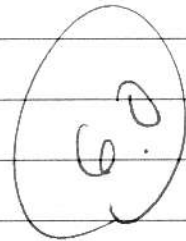
Steady state

~~$$M \frac{d^2 y}{dt^2} = F - ky - b \frac{dy}{dt}$$~~

~~$$F = ky$$~~

~~$$y = \frac{F}{k} = \frac{1 \text{ N}}{30 \text{ N/m}}$$~~

~~$$\boxed{y = 33.3 \text{ mm}}$$~~



$$T_s = \frac{4}{2 \omega_n} \quad \text{since } \delta = 2\%$$

$$2 \omega_n = +4.17 \text{ from } T_x F_n$$

$$2 \omega_n = 2.085$$

$$\rightarrow T_s = \frac{4}{2.085}$$

$$\boxed{T_s = 1.918 \text{ s}}$$

3)

Discuss stability &amp; ess for step &amp; ramp I/P



$$a) P(s) = \frac{161}{(s+5)(s+4)} = \frac{161}{s^2+9s+20}$$

$$\frac{Y}{F} = \frac{P}{1+P} = \frac{\frac{161}{(s+5)(s+4)}}{1 + \frac{161}{(s+5)(s+4)}} = \frac{161(s+5)(s+4)}{(s+5)(s+4) + 161}$$

$$Y = \frac{161}{s^2+9s+181} \quad s_{1,2} = \frac{-9 \pm \sqrt{9^2 - 4(1)(181)}}{2}$$

$$s_{1,2} = \frac{-9 \pm \sqrt{643}}{2}$$

System is stable since  $s_{1,2}$  both in LHS plane and no unstable pole zero cancellations.

Step I/P ess

Type 0 system

∴ ess to step is  $ess = \frac{1}{1+K_p}$

$$\text{where } K_p = \lim_{s \rightarrow 0} G(s) = \lim_{s \rightarrow 0} \frac{161}{s^2+9s+20} = \frac{161}{20} = 8.05$$

$$ess = \frac{1}{1+8.05} = 0.11 \Rightarrow \boxed{ess_{\text{step I/P}} = 11\%}$$

Not too bad for stability.

Ramp I/P ess

Type 0 system

∴ ess to ramp I/P is  $\infty$

$$\boxed{ess = \infty}$$

System will never reach a steady state with a ramp I/P and stable in that case.

$$Y(s) = \frac{1}{s} \frac{161}{s^2+9s+181}$$

using F.U.T.

$$\lim_{t \rightarrow \infty} y(t) = \lim_{s \rightarrow 0} s \frac{161}{s^2+9s+181} = \boxed{\infty}$$

3)

$$b) P(s) = \frac{192}{s(s+5)(s+4)} = \frac{192}{s(s^2+9s+20)} = \frac{192}{s^3+9s^2+20s}$$

$$T(s) = \frac{Y(s)}{U(s)} = \frac{P(s)}{1+P(s)} = \frac{192}{s(s+5)(s+4) + 192} = \frac{192}{s^3+9s^2+20s+192}$$

$$Y(s) = \frac{192}{s^3+9s^2+20s+192}$$

Routh Hurwitz

$s_3$	1	20	0	$\frac{1(192) - 9(20)}{-1} = -1.333$
$s_2$	9	192	0	
$s_1$	-1.333	0		
$s_0$	192	0		

System is not stable

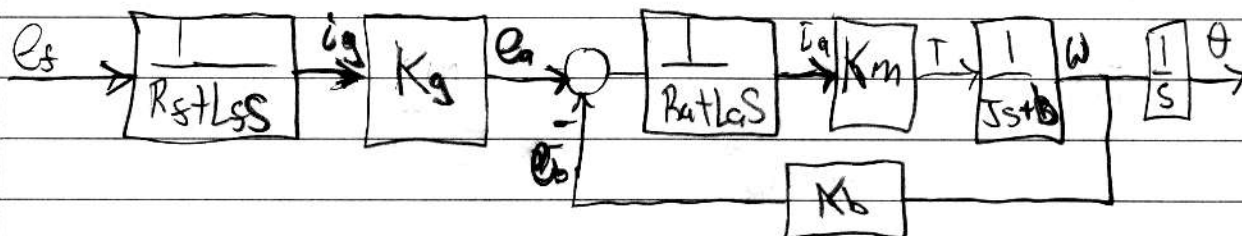
Since all left hand column entries don't have the same sign the system has poles in RHS and is unstable.

Since unstable you don't care about ess since it is unstable

6.0

4) Armature controlled DC motor.  
 generator constant speed  $\omega_g$  obtain  $\theta(s)$ .  
 $E_g(s)$

Assume  $E_a = K_g \omega_g$



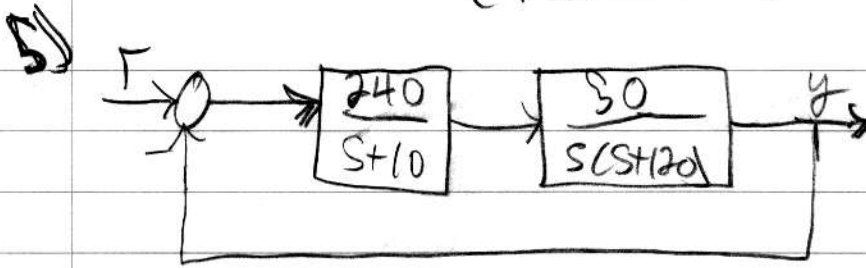
$$\frac{\theta(s)}{E_g(s)} = \frac{\left(\frac{1}{R_s + L_s s}\right) K_g \left(\frac{1}{R_a + L_a s}\right) K_m \left(\frac{1}{J s + B}\right) \frac{1}{s}}{1 + \left(\frac{1}{R_a + L_a s}\right) K_m \left(\frac{1}{J s + B}\right) K_b}$$

$$\theta(s) = \frac{K_a K_m}{s (R_s + L_s s) (R_a + L_a s) (J s + B)} \frac{(R_a + L_a s) (J s + B)}{(R_a + L_a s) (J s + B) + K_m K_b}$$

$$\theta(s) = \frac{K_g K_m}{s (R_s + L_s s) [(R_a + L_a s) (J s + B) + K_m K_b]}$$

(6.0)

$$(-4.55246153506, -8.86198166148)$$



Find second order approx.

$$\frac{Y}{R} = \frac{12000}{s(s+10)(s+20)} = \frac{12000}{s(s+10)(s+20) + 12000}$$

$$Y(s) = \frac{12000}{s^3 + 30s^2 + 1200s + 12000}$$

Roots

$$s_{1,2} = -4.55 \pm j 8.86 \quad s_3 = -120.9$$

All roots are in LHS  $\Rightarrow$  system stable  $\star$

$s_3$  of  $-120.9$  is  $\gg 10 (s_{1,2})$  So ignore  $s$  portion we then get:

$$\frac{Y(s)}{R(s)} = \frac{12000}{(s + 4.55 + j 8.86)(s + 4.55 - j 8.86)(120.9)}$$

$$\frac{Y(s)}{R(s)} = \frac{99.26}{(s + 4.55 + j 8.86)(s + 4.55 - j 8.86)}$$

$$s = -\zeta \omega_n \pm j \omega_n \sqrt{1 - \zeta^2}$$

- Find  $P.O.$ ,  $T_s$  ( $\delta = 2\%$ ),  $T_p$  and ess to step & ramp I/P's

$$T_p = \frac{\pi}{\omega_n \sqrt{1 - \zeta^2}} = \frac{\pi}{8.86198166148} = \boxed{0.355s}$$

$$T_s = \frac{4}{\zeta \omega_n} = \frac{4}{4.55246153506} = \boxed{0.879s}$$

$$\zeta \omega_n = 4.55246153506$$

$$\omega_n = \frac{4.55246153506}{\zeta} \quad \text{Next page}$$

Since  $\omega_n = 4.55246$

$$\omega_n \sqrt{1-z^2} = 8.86198$$

$$\frac{4.55246}{z} \sqrt{1-z^2} = 8.86198$$

$$\left( \frac{z \cdot 8.86198}{4.55246} \right)^2 = 1-z^2$$

(6.0)

$$z^2 \left( 1 + \left( \frac{8.86198}{4.55246} \right)^2 \right) = 1$$

$$z^2 = \frac{1}{1 + \left( \frac{8.86198}{4.55246} \right)^2} = 0.4569$$

$$P.O. = e^{\left( \frac{-z\pi}{\sqrt{1-z^2}} \right)} = e^{\left( \frac{-0.4569\pi}{\sqrt{1-(0.4569)^2}} \right)} \times 100$$

**P.O. = 19.9%**

Order of system is 1 so

Step I/P

$e_{ss} = 0$  ✓

$$K_p = \lim_{s \rightarrow 0} G(s) = \lim_{s \rightarrow 0} \frac{240 \cdot 150}{(s+10)(s+20)(s)} = \infty$$

$e_{ss} = \frac{1}{1+\infty} = 0$

Ramp I/P

$e_{ss} = 1/K_v$

$$K_v = \lim_{s \rightarrow 0} s \frac{240(150)}{s(s+10)(s+20)} = \frac{240(150)}{(10)(20)} = 10$$

$e_{ss} = 1/10 = 0.1$

= 10

**$e_{ss} = 10\%$**  ✓ fairly good steady state error